

# A parametric study on the initial transverse stability of suspension ships

CoTech#90

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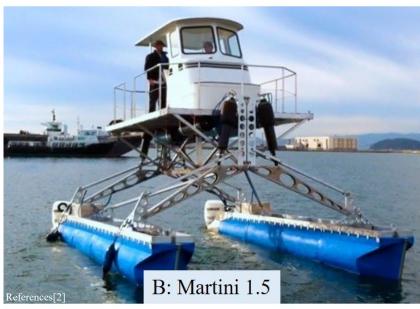
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## Introduction

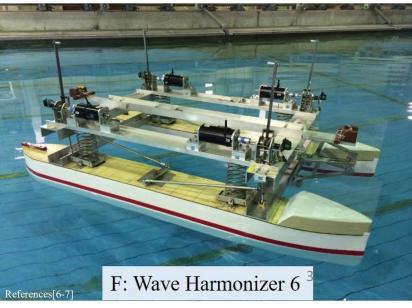






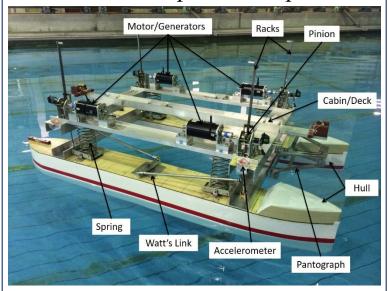






#### Introduction

What is a suspension ship?

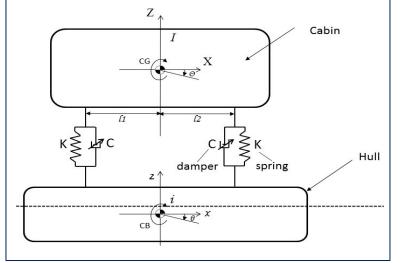


- ✓ 9 degree-of-freedom;
- ✓ Heave, pitch, and roll motions of the cabin are separable from those motions of the hull; while relative yaw, sway, and surge between the two are constrained;
- ✓ The motion of the cabin and the hull can be modified by using appropriate control systems.

• Why use suspensions on a ship?







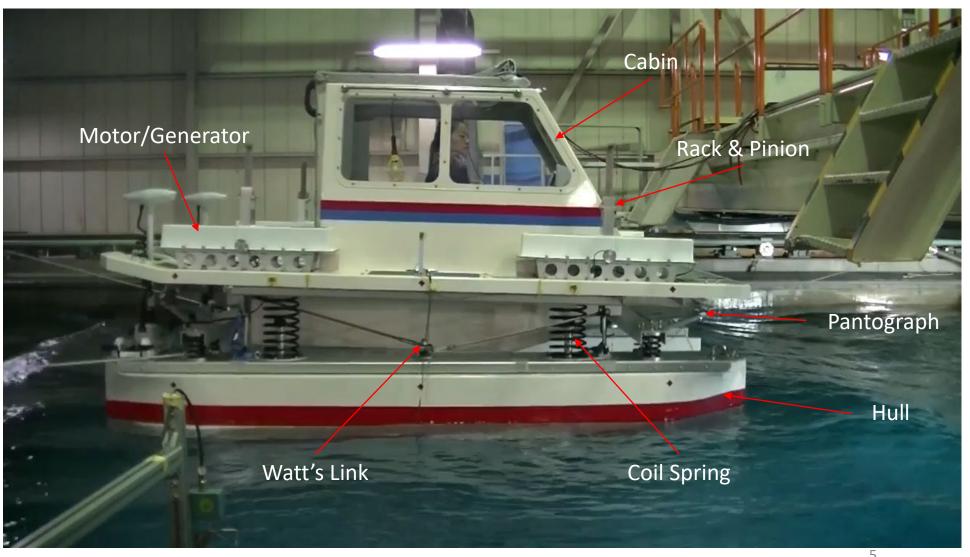
• What are the objectives of this study?



- ✓ Several types of suspension ships have been developed and tested in a towing tank.
- Control strategies have been proposed and verified in those experiments.
- ☐ Investigate characteristics of the initial transverse stability of suspension ships;
- ☐ Provide a deeper insight into the structure design of suspension ships.

## Design Principle of Suspension Ships

Safe & Comfortable



## Feature of suspension ships

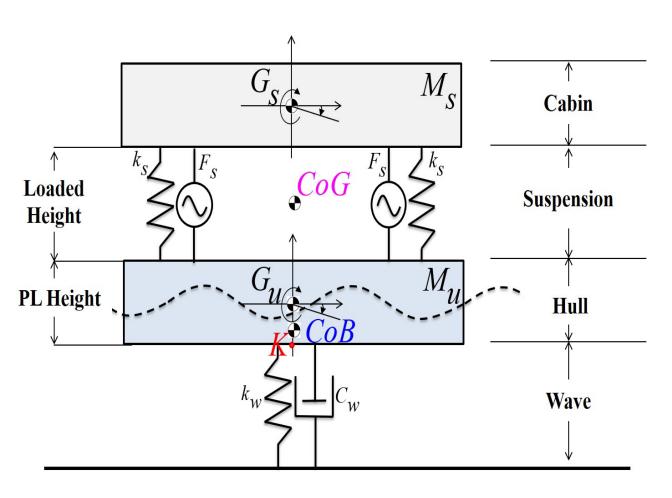


Fig.1 Structure diagram of suspension ships.

• Dynamic Mass ratio:

$$q = \frac{M_S}{M_u}$$

Ms: Sprung mass; Mu: Unsprung mass

Static Mass ratio:

$$p' = \frac{M_{cabin}}{M_{hull}}$$

 $M_{cabin}$ : mass of cabin;  $M_{chull}$ : mass of hull;

Loaded Height:

$$H_L(k_s, L_f, M_s)$$

 $k_s$ : spring stiffness;  $L_f$ : free length of spring

• Placement Location Height:

$$H_{PL}$$

**Beam of Ship**:

$$B_{hull}$$
,  $BoA$ 

## Initial Transverse Stability (GM)

Table 1. Design specifications of a suspension model

Item	Value
mass of cabin $M_1$	$2.5\mathrm{kg}$
mass of suspension $M_3$	$2.6\mathrm{kg}$
mass of hull $M_2$	$1.3\mathrm{kg}$
spring stiffness $k_s$	$235\mathrm{N/m}$
free length of spring $L_f$	$0.22\mathrm{m}$
Diameter of spring	$0.05\mathrm{m}$
Dimension of cabin $L_1, H_1, B_1$	$L0.5\mathrm{m}\ H0.20\mathrm{m}\ B0.15\mathrm{m}$
Dimension of hull $L_2, H_2, B_2$	L0.5 m H0.15 m B0.15 m

Metacentric height GM:

$$GM = KB + BM - KG$$

where, 
$$KB = \frac{d}{2}$$
,  $BM = \frac{I_L}{\nabla}$ ,  $KG = \frac{M_1 K G_1 + M_2 K G_2 + M_3 K G_3}{M_1 + M_2 + M_3}$ 

$$GM = -0.2387 < 0$$
 unstable!

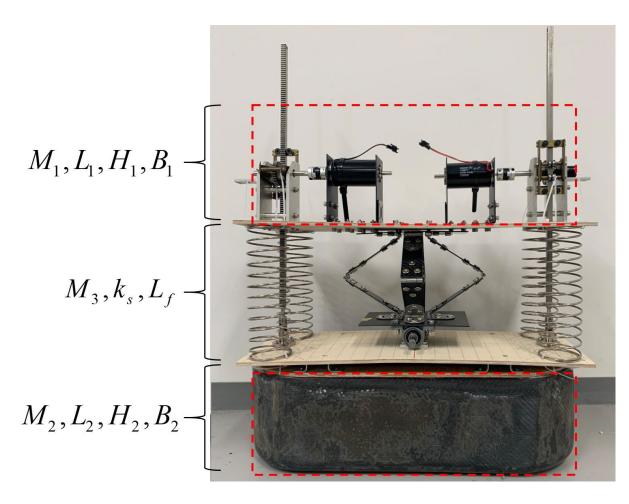
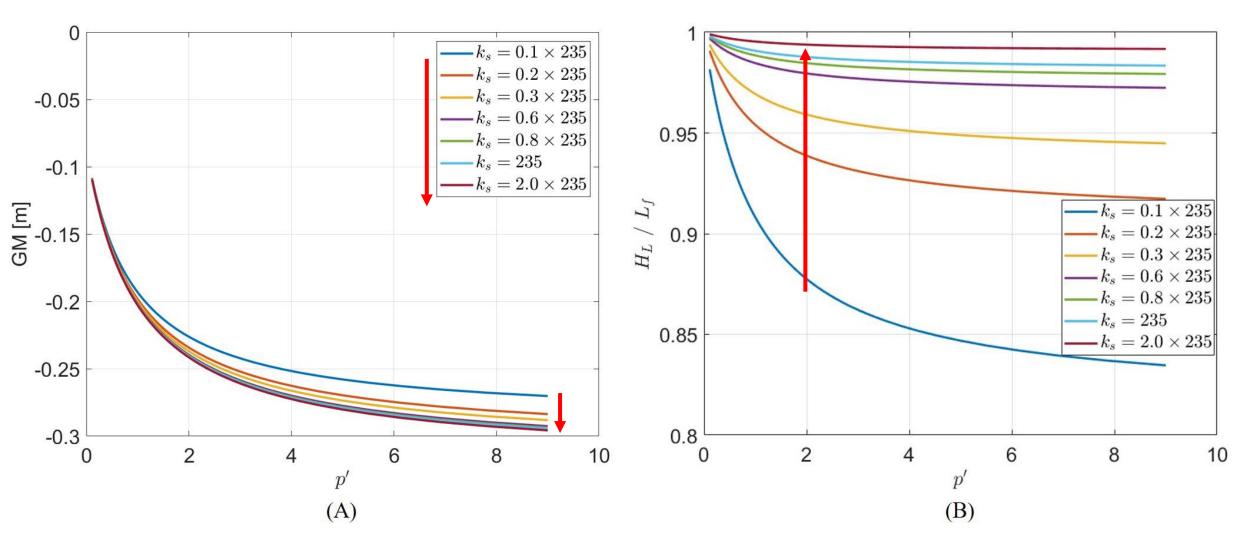


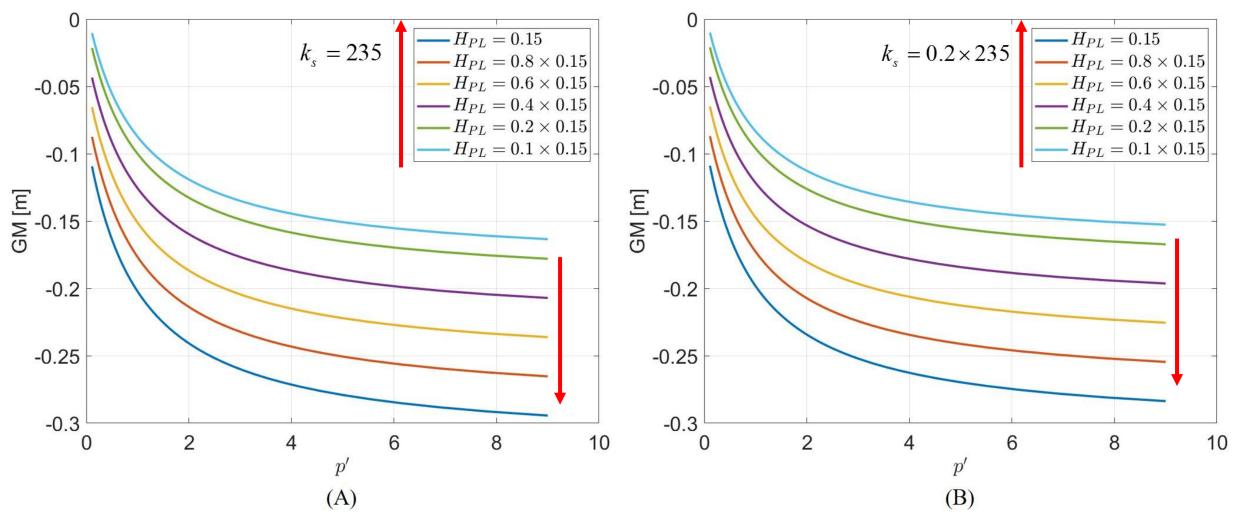
Fig.2 A prototype of suspension ship.

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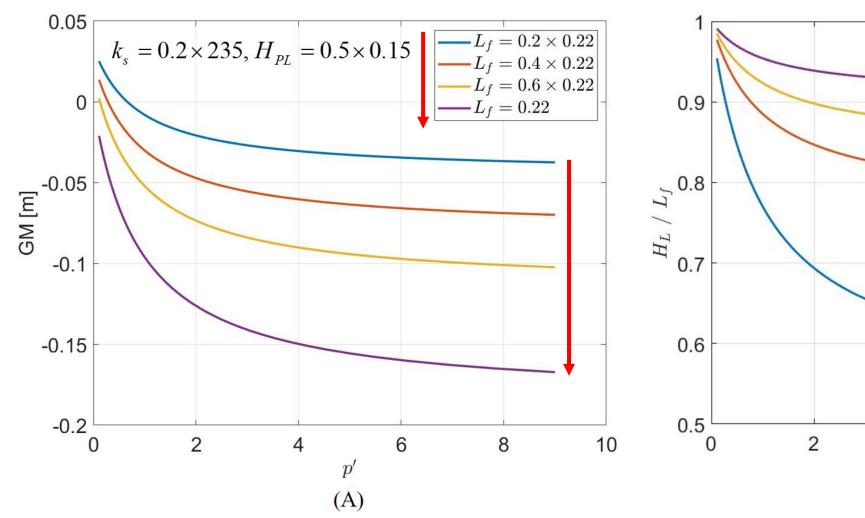
# Parametric Study (k<sub>s</sub>, M<sub>cabin</sub>/M<sub>hull</sub>)

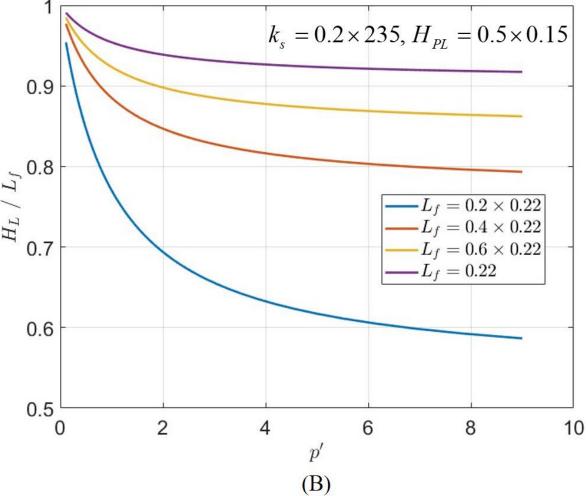


## Parametric Study (H<sub>PL</sub>, k<sub>s</sub>, M<sub>cabin</sub>/M<sub>hull</sub>)

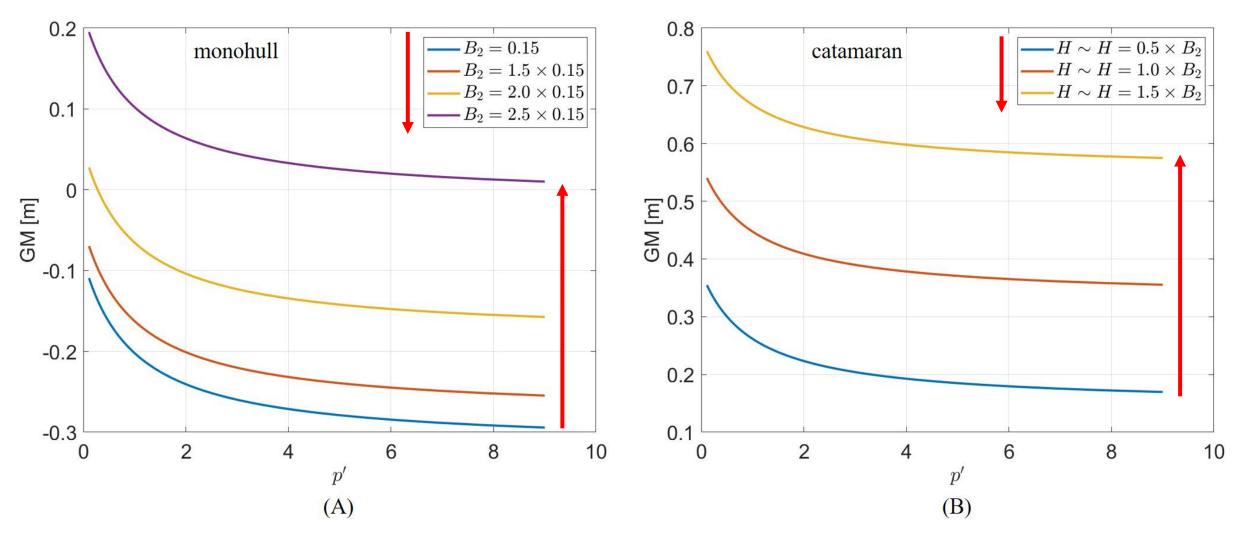


## Parametric Study (L<sub>f</sub>, M<sub>cabin</sub>/M<sub>hull</sub>)





## Parametric Study (Beam of ship)



### Conclusions:

- 1. A reduced mass ratio results in an increased GM. The initial transverse stability displays significant variation when the mass ratio of the cabin and hull is **less than 2**. It is imperative to pay close attention if the static mass ratio falls within this range;
- 2. A **shorter** loaded height is preferable for a larger GM. However, the allowable travel distance must be taken into account to prevent bottom out. If springs are utilized, the spring stiffness and free length must be carefully balanced.
- 3. A **lower** placement location height results in a larger GM. Although, the impact becomes weaker with the reduced static mass ratio, it exerts more impact compared to the spring stiffness.
- 4. A **larger** beam produces a larger GM. The beam of the hull for a monohull and the overall beam of a catamaran are the dominating parameters that influence the initial transverse stability.

# Thank you for your attention!

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